Uddeholm Orvar[®] Supreme



Uddeholm Orvar® Supreme

Uddeholm Orvar Supreme can be regarded as an "all-round" steel used in several application areas. Except for hot work application areas the steel is also used in moulds for plastics and as a material in high stressed axles.

The high degree of purity and the very fine structure shows improvement in dies and components where high mechanical and thermal stresses are involved.

Uddeholm Orvar Supreme is produced using the Electro-Slag-Refining (ESR) technique. The ESR process gives Orvar Supreme a high level of homogeneity and cleanliness which results in a high performance hot work tool steel of the highest quality.

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This information is based on our present state of knowledge and is intended to provide general notes on our products and their uses. It should not therefore be construed as a warranty of specific properties of the products described or a warranty for fitness for a particular purpose.

Classified according to EU Directive 1999/45/EC For further information see our "Material Safety Data Sheets". ES 9001 · OHSAS 18001 ISO 14001 · ISO 50001

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GENERAL

Uddeholm Orvar Supreme is a Superior type ESR AISI H13 which fits in the NADCA#207, Grade B band. It is a chromium-molybdenum-vanadium-alloyed steel characterized by:

- High level of resistance to thermal shock and thermal fatigue
- Good high-temperature strength
- Uddeholm Orvar Supreme is rated to the higher level of cleanliness in NADCA#207 for Superior ESR AISI H13, Grade B.
- Excellent toughness and ductility in all directions
- Uddeholm Orvar Supreme is rated to Min/avg 16J/12ft-lbs in as delivered condition
- · Good machinability and polishability
- · Excellent through-hardening properties
- Good dimensional stability during hardening

Typical analysis %	C 0.39	Si 1.0	Mn 0.4	Cr 5.2	Mo 1.4	V 0.9
Standard specification	Superior AISI H13 per NADCA#207 Grade E				irade B	
Delivery condition	Soft annealed to approx. 180 HB					
Toughness	Orvar Supreme exceeds the NADCA B specification for Min/Avg toughness at 16J/12ft-lbs					
Colour code	Orange					

IMPROVED TOOLING PERFORMANCE

The name "Supreme" implies that by special processing techniques and close control, the steel attains high purity and a very fine structure. Further, Uddeholm Orvar Supreme shows significant improvements in isotropic properties compared to conventionally produced AISI H13 grades.

These improved isotropic properties are particularly valuable for tooling subjected to high mechanical and thermal fatigue stresses, e.g. die casting dies, forging tools and extrusion tooling. In practical terms, tools may be used at somewhat higher working hardnesses (+1 to 2 HRC) without loss of toughness. Since in-creased hardness slows down the formation of heatchecking cracks, improved tool performance can be expected.

Uddeholm Orvar Supreme meets the North American Die Casting Association (NADCA) #207 requirements for Superior high quality H-13 die steel. This requires the steel to have a minimum average toughness of \geq 10ft-lbs as tested in soft annealed delivered condition.

However, Uddeholm Orvar Supreme is rated higher in the Min/Avg test by Uddeholm. It exceeds the NADCA#207, Grade B, Min/ Avg specification in soft annealed delivered toughness to 16 Joules or 12ft-lbs.

APPLICATIONS

TOOLS FOR DIE CASTING

Part	Tin, lead zinc alloys HRC	Aluminium, magnesium alloys, HRC	Copper alloys HRC
Dies Fixed inserts	46–50	42–48	(QRO 90 S)
cores	46–52	44–48	(QRO 90 S)
Sprue parts	48–52	46–48	(QRO 90 S)
Nozzles	35–42	42–48	(QRO 90 S)
Ejector pins (nitrided) Plunger, shot-sleeve (normally nitrided)	46-50	46-50	46–50 (QRO 90 S)
Tildidedj	42-40	42-40	
Austenitizing temperature		–1030°C –1885°F)	1040–1050°C (1900–1920°F)

TOOLS FOR EXTRUSION

Part	Aluminium, magnesium alloys, HRC	Copper alloys HRC	Stainless steel HRC
Dies Backers, die- holders, liners, dummy blocks, stems	44–50 41–50	43–47 40–48	45–50 40–48
Austenitizing temperature (approx.)	1020–1030°C (1870–1885°F)		–1050°C –1920°F)

TOOLS FOR FORGING

Material	Aust. temp. (approx.)	HRC
Aluminium, magnesium Copper alloys Steel	1020–1030°C (1870–1885°F) 1040–1050°C (1900–1920°F) 1040–1050°C (1900–1920°F)	44–52 44–52 50–52



MOULDS FOR PLASTICS

Part	Austenitizing temp.	HRC
Injection moulds Compression/	1020–1030°C (1870–1885°F)	
transfer moulds	Tempering 1. ≥ 550°C (1020°F) or 2. 250°C (480°F)	40–52 50–53

OTHER APPLICATIONS

Application	Austenitizing temp.	HRC
Severe cold punching, scrap shears	1020–1030°C (1870–1885°F) Tempering 250°C (480°F)	50–53
Hot shearing	1020–1030°C (1870–1885°F) Tempering 1. 250°C (480°F) or 2. 575–600°C (1070–1110°F)	50–53 45–50
Shrink rings (e.g. for cemented carbide dies)	1020–1030°C (1870–1885°F) Tempering 575–600°C (1070–1110°F)	45–50
Wear- resisting parts	1020–1030°C (1870–1885°F) Tempering 575°C (1070°F) Nitriding	Core 50–52 Surface ~1000HV ₁

PROPERTIES

All specimens are taken from the centre of a 407 x 127 mm (16" x 5") bar. Unless otherwise is indicated all specimens were hardened 30 minutes at 1025°C (1875°F), quenched in air and tempered 2 + 2 h at 610°C (1130°F). The hardness were 45 ± 1 HRC.

PHYSICAL DATA

Data at room and elevated temperatures.

Temperature	20°C	400°C	600°C
	(68°F)	(750°F)	(1110°F)
Density			
kg/m ³	7 800	7 700	7 600
lbs/in ³	0.281	0.277	0.274
Modulus of			
elasticity MPa	210 000	180 000	140 000
psi	30.5 x 10 ⁶	26.1 x 10 ⁶	20.3 x 10 ⁶
- po.		2011 X 10	2010 / 10
Coefficient of			
thermal expan-			
sion per °C from 20°C	_	12.6 x 10⁻⁵	13.2 x 10 ⁻⁶
°F from 68°F	_	7.0 x 10 ⁻⁶	7.3 x 10 ⁻⁶
Thermal			
conductivity			
W/m °C	25	29	30
Btu in/(ft ² h°F)	176	204	211
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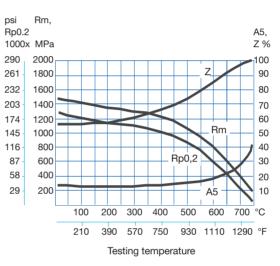
MECHANICAL PROPERTIES

Approximate tensile strength at room temperature.

Hardness	52 HRC	45 HRC
Tensile strength Rm	1820 MPa 185 kp/mm² 117 tsi 263 000 psi	1420 MPa 145 kp/mm² 92 tsi 206 000 psi
Yield strength Rp0.2	1520 MPa 155 kp/mm² 98 tsi 220 000 psi	1280 MPa 130 kp/mm² 83 tsi 185 000 psi

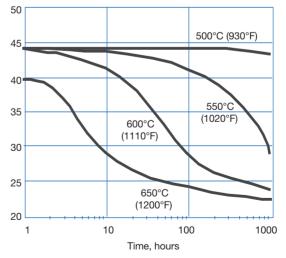
APPROXIMATE STRENGTH AT ELEVATED TEMPERATURES

Longitudinal direction.



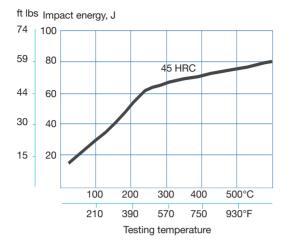
EFFECT OF TIME AT HIGH TEMPERATURES ON HARDNESS

Hardness, HRC



EFFECT OF TESTING TEMPERATURE ON IMPACT ENERGY

Charpy V specimens, short transverse direction.



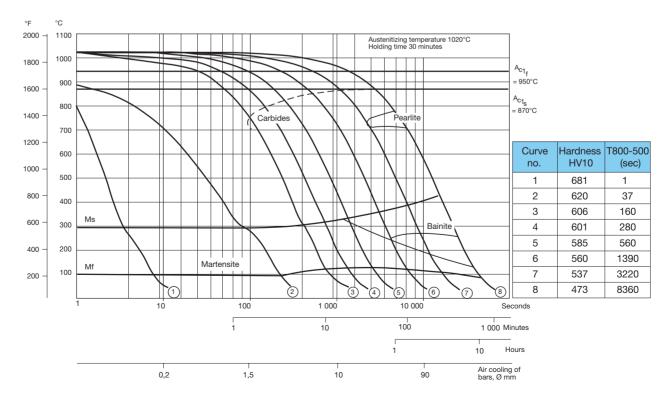
HEAT TREATMENT – GENERAL RECOMMENDATIONS

SOFT ANNEALING

Protect the steel and heat through to 850°C (1560°F). Then cool in the furnace at 10°C (20°F) per hour to 650°C (1200°F), then freely in air.

CCT GRAPH

Austenitizing temperature 1020°C (1870°F). Holding time 30 minutes.



STRESS RELIEVING

After rough machining the tool should be heated through to 650°C (1200°F), holding time 2 hours. Cool slowly to 500°C (930°F), then freely in air.

HARDENING

Pre-heating temperature: 600–850°C (1110–1560°F), normally in two pre-heating steps.

Austenitizing temperature: 1020–1050°C (1870–1920°F), normally 1020–1030°C (1870–1885°F).

Tempo	erature	Soaking* time	Hardness before
°C	°F	minutes	tempering
1025	1875	30	53±2 HRC
1050	1920	15	54±2 HRC

* Soaking time = time at hardening temperature after the tool is fully heated through

Protect the part against decarburization and oxidation during hardening.

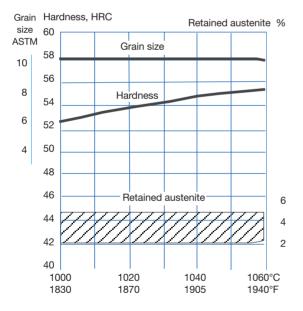
QUENCHING MEDIA

- High speed gas/circulating atmosphere
- Vacuum (high speed gas with sufficient positive pressure). An interrupted quench is recommended where distortion control and quench cracking are a concern
- Martempering bath or fluidized bed at 450–550°C (840–1020°F), then cool in air
- Martempering bath or fluidized bed at approx. 180–220°C (360–430°F) then cool in air
- Warm oil

Note 1: Temper the tool as soon as its temperature reaches 50–70°C (120–160°F).

Note 2: In order to obtain the optimum properties for the tool, the cooling rate should be fast, but not at a level that gives excessive distortion or cracks.

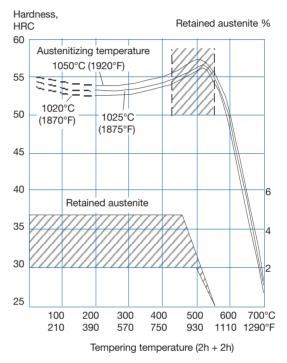
HARDNESS, GRAIN SIZE AND RETAINED AUSTENITE AS FUNCTIONS OF AUSTENITIZING TEMPERATURE



TEMPERING

Choose the tempering temperature according to the hardness required by reference to the tempering graph. Temper minimum twice with intermediate cooling to room temperature. Lowest tempering temperature 250°C (480°F). Holding time at temperature minimum 2 h. To avoid "temper brittleness", do not temper in the range 425–550°C (800–1020°F), see graph.

TEMPERING GRAPH

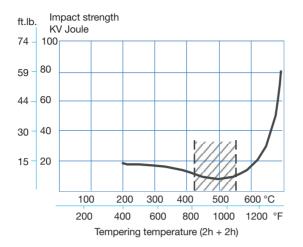


Above tempering curves are obtained after heat treatment of samples with a size of $15 \times 15 \times 40$ mm, cooling in forced air. Lower hardness can be expected after heat treatment of tools and dies due to factors like actual tool size and heat treatment parameters.



APPROXIMATE IMPACT STRENGTH AT DIFFERENT TEMPERING TEMPERATURES Charpy V specimens, short transverse

direction.



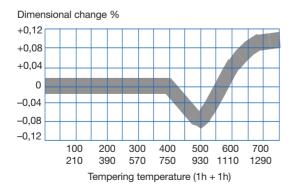
Tempering within the range 425–550°C (800–1020°F) is normally not recommended due to the reduction in toughness properties.

DIMENSIONAL CHANGES DURING HARDENING

Sample plate, 100 x 100 x 25 mm, 4" x 4" x 1".

		Width %	Length %	Thickness %
Oil hardened from				
	Min.	-0.08	-0.06	±0
1020°C (1870°F)	Max.	-0.15	-0.16	+0.30
Air hardened from				
	Min.	-0.02	-0.05	±0
1020°C (1870°F)	Max.	+0.03	+0.02	+0.05
Vac hardened from				
	Min.	+0.01	-0.02	+0.08
1020°C (1870°F)	Max.	+0.02	-0.04	+0.12

DIMENSIONAL CHANGES DURING TEMPERING



Note: The dimensional changes in hardening and tempering should be added.

NITRIDING AND NITROCARBURIZING

Nitriding and nitrocarburizing result in a hard surface layer which is very resistant to wear and erosion. The nitrided layer is, however, brittle and may crack or spall when exposed to mechanical or thermal shock, the risk increas-ing with layer thickness. Before nitriding, the tool should be hardened and tempered at a temperature at least 25–50°C (45–90°F) above the nitriding temperature.

Nitriding in ammonia gas at 510° C (950°F) or plasma nitriding in a 75% hydrogen/25% nitrogen mixture at 480°C (895°F) both result in a surface hardness of about 1100 HV_{0.2}. In general, plasma nitriding is the preferred method because of better control over nitrogen potential; in particular, formation of the so-called white layer, which is not recommended for hot-work service, can readily be avoided. However, careful gas nitriding can give perfectly acceptable results.

Uddeholm Orvar Supreme can also be nitrocarburized in either gas or salt bath.The surface hardness after nitrocarburizing is 900–1000 HV_{0.2}.

		Depth		
Process	Time	mm	inch	
Gas nitriding at 510°C (950°F)	10 h 30 h	0.12 0.20	0.0047 0.0079	
Plasma nitriding at 480°C (895°F)	10 h 30 h	0.12 0.18	0.0047 0.0071	
Nitrocarburizing – in gas at				
580°C (1075°F) – in salt bath at	2.5 h	0.11	0.0043	
580°C (1075°F)	1 h	0.06	0.0024	

Nitriding to case depths >0.3 mm (>0.012 inch) is not recommended for hot work applications. Uddeholm Orvar Supreme can be nitrided in the soft-annealed condition. The hardness and depth of case will, however, be reduced somewhat in this case.

DEPTH OF NITRIDING

MACHINING RECOMMENDATIONS

The cutting data below are to be considered as guiding values, which must be adapted to existing local conditions.

More information can be found in the Uddeholm publication "Cutting data recommendation".

TURNING

Cutting data parameters	Turning with carbide Rough Fine turning turning		Turning with high speed steel Fine turning
Cutting speed (v _c) m/min f.p.m.	200–250 660–820	250–300 820–985	25–30 82–100
Feed (f) mm/r i.p.r.	0.2–0.4 0.008–0.016	0.05–0.2 0.002–0.008	0.05–0.3 0.002–0.012
Depth of cut (a _p) mm inch	2–4 0.08–0.16	0.5–2 0.02–0.08	0.5–2 0.02–0.08
Carbide designation ISO	P20–P30 Coated carbide	P10 Coated carbide or cermet	_

DRILLING

HIGH SPEED STEEL TWIST DRILL

Drill diameter		Cutting speed, v_c		Feed, f	
mm	inch	m/min	f.p.m.	mm/r	i.p.r.
- 5	-3/16	16–18*	52–59*	0.05-0.15	0.002-0.006
5–10	3/16–3/8	16–18*	52–59*	0.15–0.20	0.006-0.008
10–15	3/8–5/8	16–18*	52–59*	0.20-0.25	0.008-0.010
15–20	5/8–3/4	16–18*	52–59*	0.25–0.35	0.010-0.014

 * For coated high speed steel drill v_ = 28–30 m/min (92–98 f.p.m.)

CARBIDE DRILL

	Type of drill		
Cutting data parameters	Indexable insert	Solid carbide	Carbide tip ¹⁾
Cutting speed (v _c) m/min f.p.m.	220–240 720–785	130–160 425–525	80–110 260–360
Feed (f) mm/r i.p.r.	0.03–0.12 ²⁾ 0.001–0.005 ²⁾	0.08–0.20 ³⁾ 0.003–0.008 ³⁾	0.15–0.25 ⁴⁾ 0.006–0.010 ⁴⁾

¹⁾ Drill with replaceable or brazed carbide tip

^a Feed rate for drill diameter 20–40 mm (0.8"–1.6")

Feed rate for drill diameter 5–20 mm (0.2"–0.8")

Feed rate for drill diameter 10–20 mm (0.4"–0.8")

MILLING

FACE AND SQUARE SHOULDER MILLING

	Milling with carbide	
Cutting data parameters	Rough milling	Fine milling
Cutting speed (v _e) m/min f.p.m.	180–260 590–850	260–300 850–985
Feed (f _z) mm/tooth inch/tooth	0.2–0.4 0.008–0.016	0.1–0.2 0.004–0.008
Depth of cut (a _p) mm inch	2–5 0.08–0.20	-2 -0.08
Carbide designation ISO	P20–P40 Coated carbide	P10–P20 Coated carbide or cermet

END MILLING

	Type of end mill		
Cutting data parameters	Solid carbide	Carbide indexable insert	High speed steel
Cutting speed (v _c) m/min f.p.m.	160–200 525–660	170–230 560–755	35–40 ¹⁾ 115–130 ¹⁾
Feed (f _z) mm/tooth inch/tooth	0.03–0.20 ²⁾ 0.001–0.008 ²⁾	0.08–0.20 ²⁾ 0.003–0.008 ²⁾	0.05–0.35 ²⁾ 0.002–0.014 ²⁾
Carbide designation ISO	_	P20, P30	_

 $^{\rm 1)}$ For coated high speed steel end mill v_c = 55–60 m/min (180–195 f.p.m.)

²⁾ Depending on radial depth of cut and cutter diameter

GRINDING

A general grinding wheel recommendation is given below. More information can be found in the Uddeholm brochure "Grinding of Tool Steel" and can also be obtained from the grinding wheel manufacturer.

WHEEL RECOMMENDATION

Type of grinding	Soft annealed condition	Hardened condition
Face grinding straight wheel Face grinding	A 46 HV	A 46 HV
segments	A 24 GV	A 36 GV
Cylindrical grinding	A 46 LV	A 60 KV
Internal grinding	A 46 JV	A 60 IV
Profile grinding	A 100 KV	A 120 KV

WELDING

Welding of tool steel can be performed with good results if proper precautions are taken regarding elevated temperature, joint preparation, choice of consumables and welding procedure.

Welding method	TIG	MMA		
Working temperature	325–375°C 620–710°F	325–375°C 620–710°F		
Filler metal	QRO 90 TIG-WELD DIEVAR TIG-WELD QRO 90 WE			
Cooling rate	20–40°C/h (40–70°F/h) the first 2–3 h then freely in air.			
Hardness after welding	50–55 HRC	50–55 HRC		
Heat treatment after welding				
Hardened condition	Temper at 10–20°C (20–40°F) below the original tempering temperature.			
Soft annealed condition	Soft-anneal the material at 850°C (1560°F) in protected atmosphere. Then cool in the furnace at 10°C 20°F) per hour to 650°C (1200°F) then freely in air.			

More detailed information can be found in the Uddeholm brochure "Welding of Tool Steel".



ELECTRICAL DISCHARGE MACHINING – EDM

If spark-erosion is performed in the hardened and tempered condition, the white re-cast layer should be removed mechanically e.g. by grinding or stoning. The tool should then be given an additional temper at approx. 25°C (50°F) below the previous tempering temperature.

HARD-CHROMIUM PLATING

After plating, parts should be tempered at 180°C (360°F) for 4 hours within 4 hours of plating to avoid the risk of hydrogen embrittlement.

POLISHING

Uddeholm Orvar Supreme has good polishability in the hardened and tempered condition because of a very homogeneous structure. This coupled with a low level of non metallic inclusions, due to ESR process, ensures good surface finish after polishing.

Note: Each steel grade has an optimum polishing time which largely depends on hardness and polishing technique. Overpolishing can lead to a poor surface finish, "orange peel" or pitting.

Further information is given in the Uddeholm publication "Polishing of mould steel".

PHOTO-ETCHING

Uddeholm Orvar Supreme is particularly suitable for texturing by the photo-etching method. Its high level of homogeneity and low sulphur content ensures accurate and consistent pattern reproduction.

FURTHER INFORMATION

Please contact your local Uddeholm office for further information on the selection, heat treatment, application and availability of Uddeholm tool steel.

THE ESR TOOL STEEL PROCESS

The starting material for our tool steel is carefully selected from high quality recyclable steel. Together with ferroalloys and slag formers, the recyclable steel is melted in an electric arc furnace. The molten steel is then tapped into a ladle.

The de-slagging unit removes oxygen-rich slag and after the de-oxidation, alloying and heating of the steel bath are carried out in the ladle furnace. Vacuum de-gassing removes elements such as hydrogen, nitrogen and sulphur.

ESR PLANT

In uphill casting the prepared moulds are filled with a controlled flow of molten steel from the ladle.

From this, the steel can go directly to our rolling mill or to the forging press, but also to our ESR furnace where our most sophisticated steel grades are melted once again in an electro slag remelting process. This is done by melting a consumable electrode immersed in an overheated slag bath. Controlled solidification in the steel bath results in an ingot of high homogeneity, thereby removing macro segregation. Melting under a protective atmosphere gives an even better steel cleanliness.

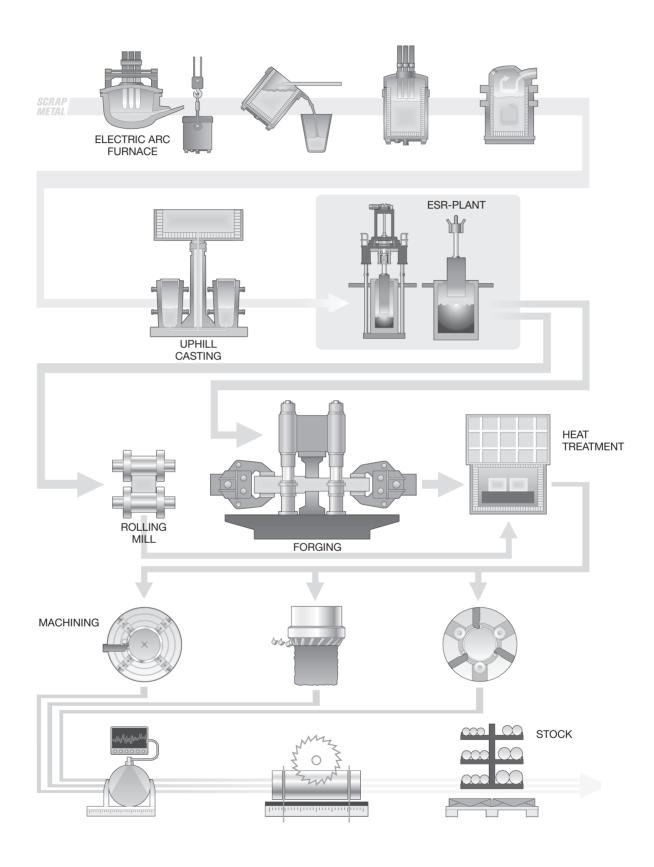
HOT WORKING

From the ESR plant, the steel goes to the rolling mill or to our forging press to be formed into round or flat bars. Prior to delivery all of the different bar materials are subjected to a heat treatment operation, either as soft annealing or hardening and tempering. These operations provide the steel with the right balance between hardness and toughness.

MACHINING

Before the material is finished and put into stock, we also rough machine the bar profiles to required size and exact tolerances. In the lathe machining of large dimensions, the steel bar rotates against a stationary cutting tool. In peeling of smaller dimensions, the cutting tools revolve around the bar.

To safeguard our quality and guarantee the integrity of the tool steel we perform both surface- and ultrasonic inspections on all bars. We then remove the bar ends and any defects found during the inspection.



Manufacturing solutions for generations to come

SHAPING THE WORLD®

We are shaping the world together with the global manufacturing industry. Uddeholm manufactures steel that shapes products used in our every day life. We do it sustainably, fair to people and the environment. Enabling us to continue shaping the world – today and for generations to come.

